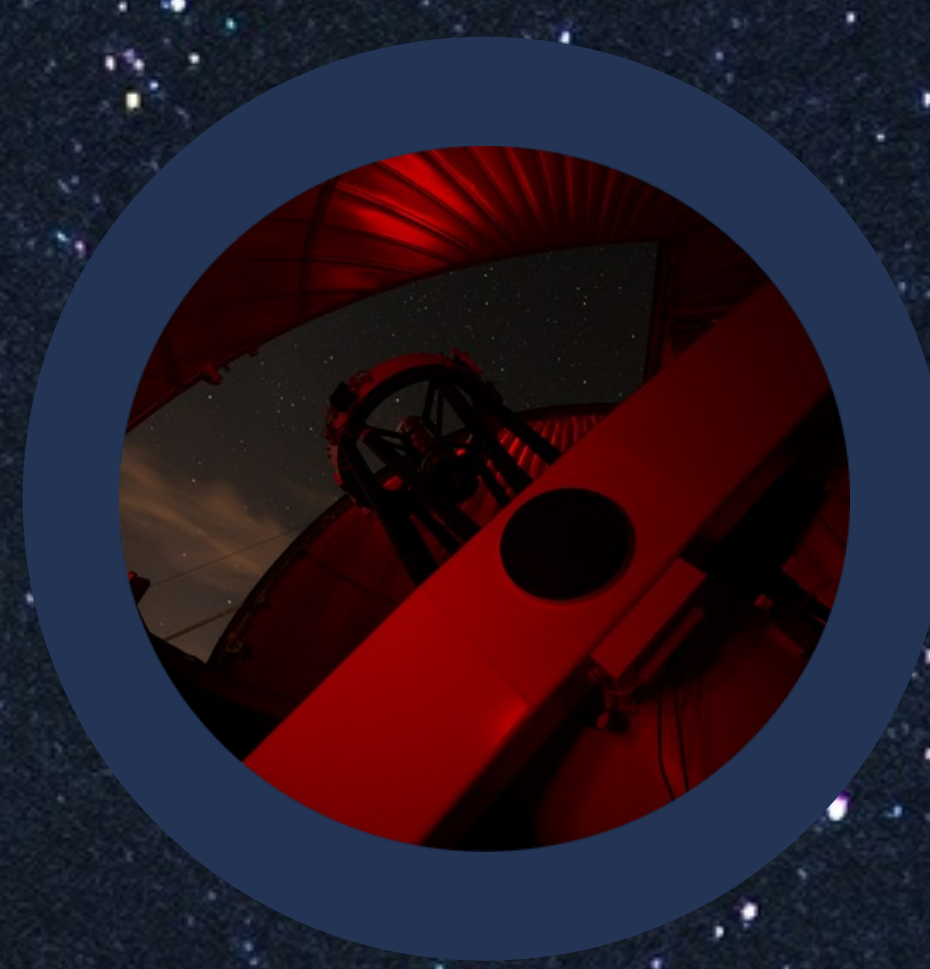


CUSTOM SHACK-HARTMANN SENSOR FOR STELLAR INTENSITY INTERFEROMETRY

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MOTIVATION

Stellar intensity interferometry (SII) benefits from narrow bandpass filters for improved $g^{(2)}$ contrast requiring fully collimated wavefronts. The Shack-Hartmann sensor ensures this by detecting and correcting wavefront distortions through spot deviation analysis.

TELESCOPE SITE

SII measurements were performed at the Calern Observatory located on a plateau in the South of France near Nice at an altitude of 1270 meters. C2PU offers twin telescopes at a separation of 15m.



Telescope Specifications:

- Primary mirror diameter: 1.04 m
- Focal length: 13 m
- Focal ratio: F/12.5
- Cassegrain secondary focus
- Equatorial yoke mount

FROM SENSOR DATA TO PRECISION

- Spot Deviations:
 - SH sensor captures deviations $(\Delta x_i, \Delta y_i)$ in spot pattern from regular grid
- Expansion:
 - wavefront W can be expanded using the Zernike polynomials

$$W(x, y) = \sum_{i=0}^3 a_i Z_i(x, y)$$

- Calculation of the minima:

- The merit function $G(\vec{a})$ is defined as

$$G(\vec{a}) = \sum_{i=0}^M \left[\left(\frac{\partial W(x_i, y_i)}{\partial x} - \frac{\Delta x_i}{f} \right)^2 + \left(\frac{\partial W(x_i, y_i)}{\partial y} - \frac{\Delta y_i}{f} \right)^2 \right]$$

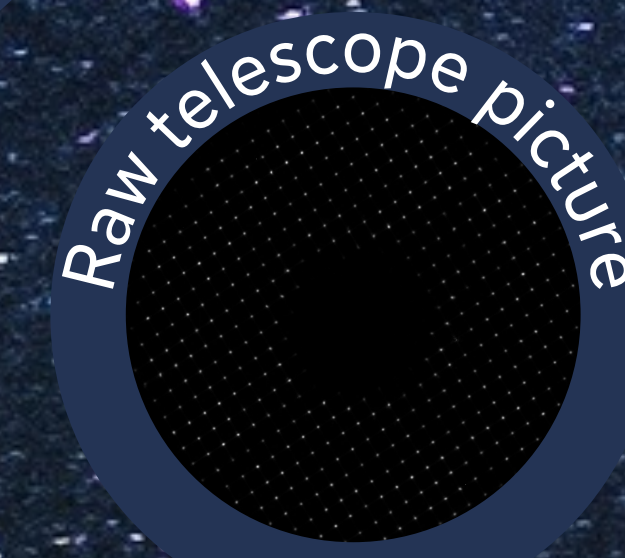
where M is the number of grid points, $\partial W(x_i, y_i) / \partial x$ is the expansion's derivative at position i and f is the focal length of a microlens

- The calculation of the minima of the merit function can be rewritten to a set of linear equations that can be solved by least-squares fitting^[1]:

$$A \cdot \vec{a} \doteq \vec{b}$$

- The result is the vector $\vec{a}$ containing the Zernike coefficients

[1] Pfund, J., Lindlein, N. and Schwider, J., 1998. Misalignment effects of the Shack-Hartmann sensor. *Applied optics*, 37(1), pp.22-27.



- Correcting Defocus:

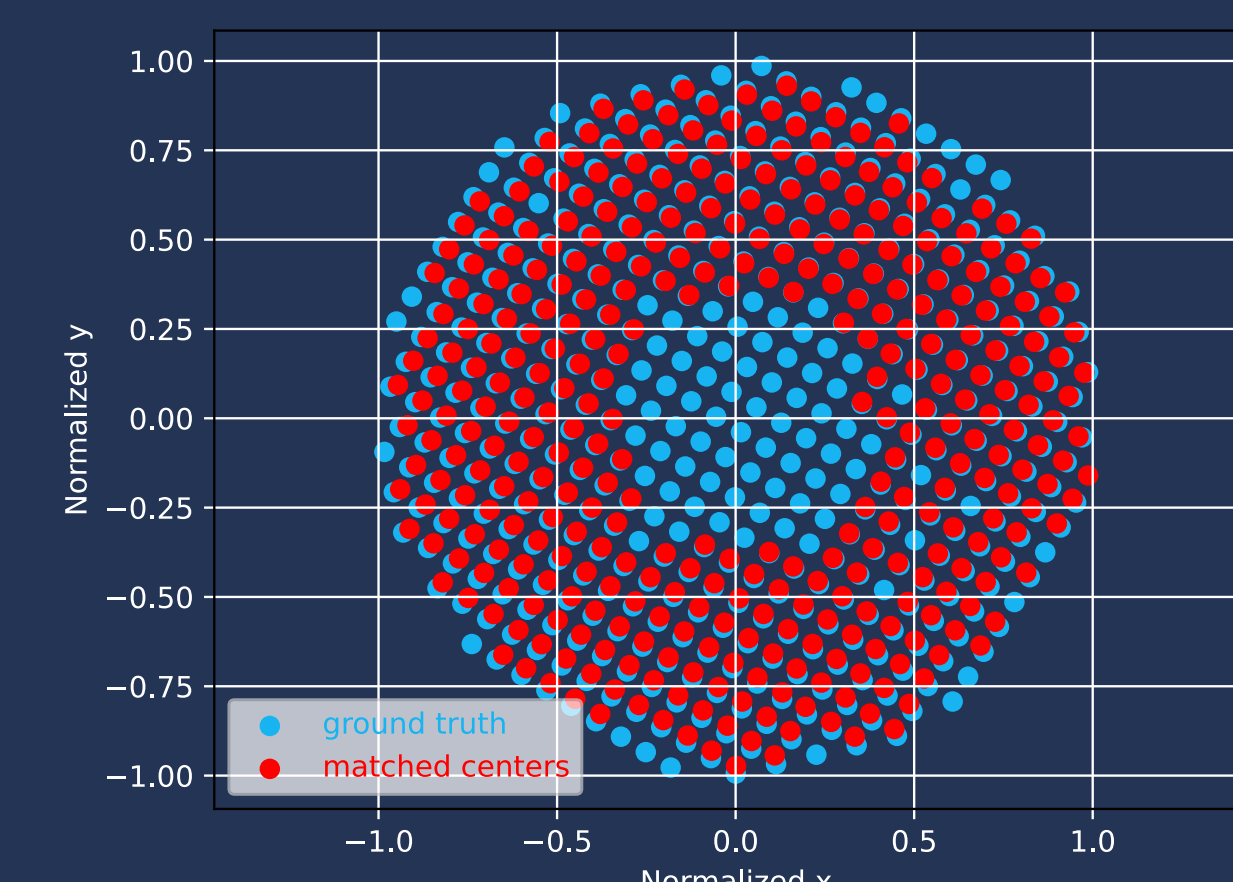
- necessary shift of secondary mirror Δz can be calculated using defocus coefficient a_3 , central wavelength of the filter λ and the numerical aperture NA :

$$\Delta z = 4a_3 \lambda / NA^2$$

- Motorized secondary mirror can move $\Delta z = \pm 23 \text{ mm}$
- The realignment moves the focal point ensuring a collimated wavefront at the filter as well as on the SH sensor

IMAGE EVALUATION

- Software reads PNG from ZWO CMOS camera and matches centers up to a certain threshold
- ideal grid is generated using the properties of the microlens array (MLA)
- ideal grid is translated and rotated to fit the matched raw image = ground truth
- coordinates are normalized to unit circle resembling the aperture diameter
- deviations from the ground truth are calculated



- deviations in x/y-direction and the coordinates are feed into the least squares fit

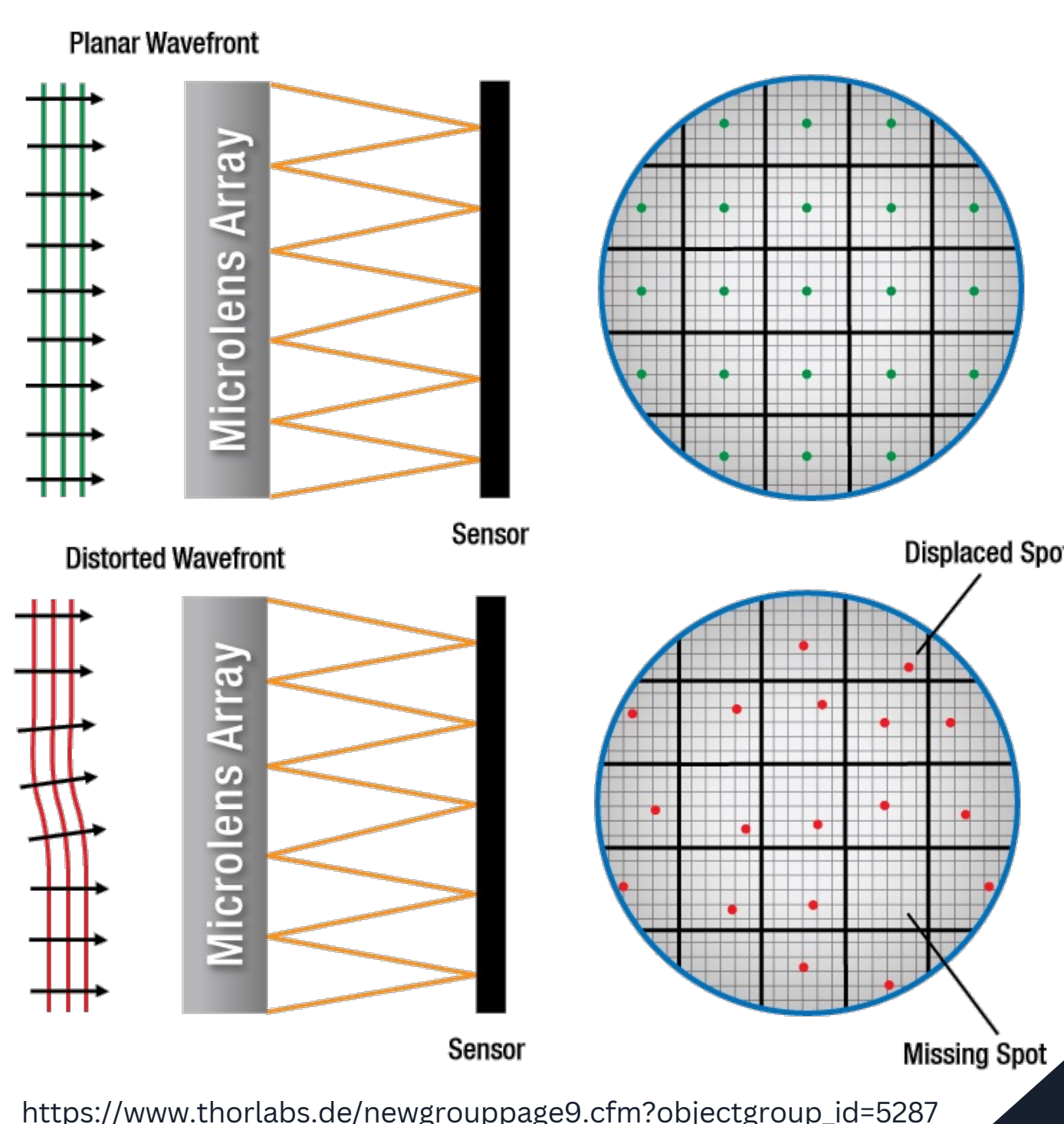
TRR 306

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BENEFITS TO THE EXPERIMENT:

- Real-time Correction: Compensates for telescope defocus, improving beam collimation and experimental accuracy.
- Scalability: Supports higher-order polynomials for future aberration correction.



https://www.thorlabs.de/newgrouppage9.cfm?objectgroup_id=5287

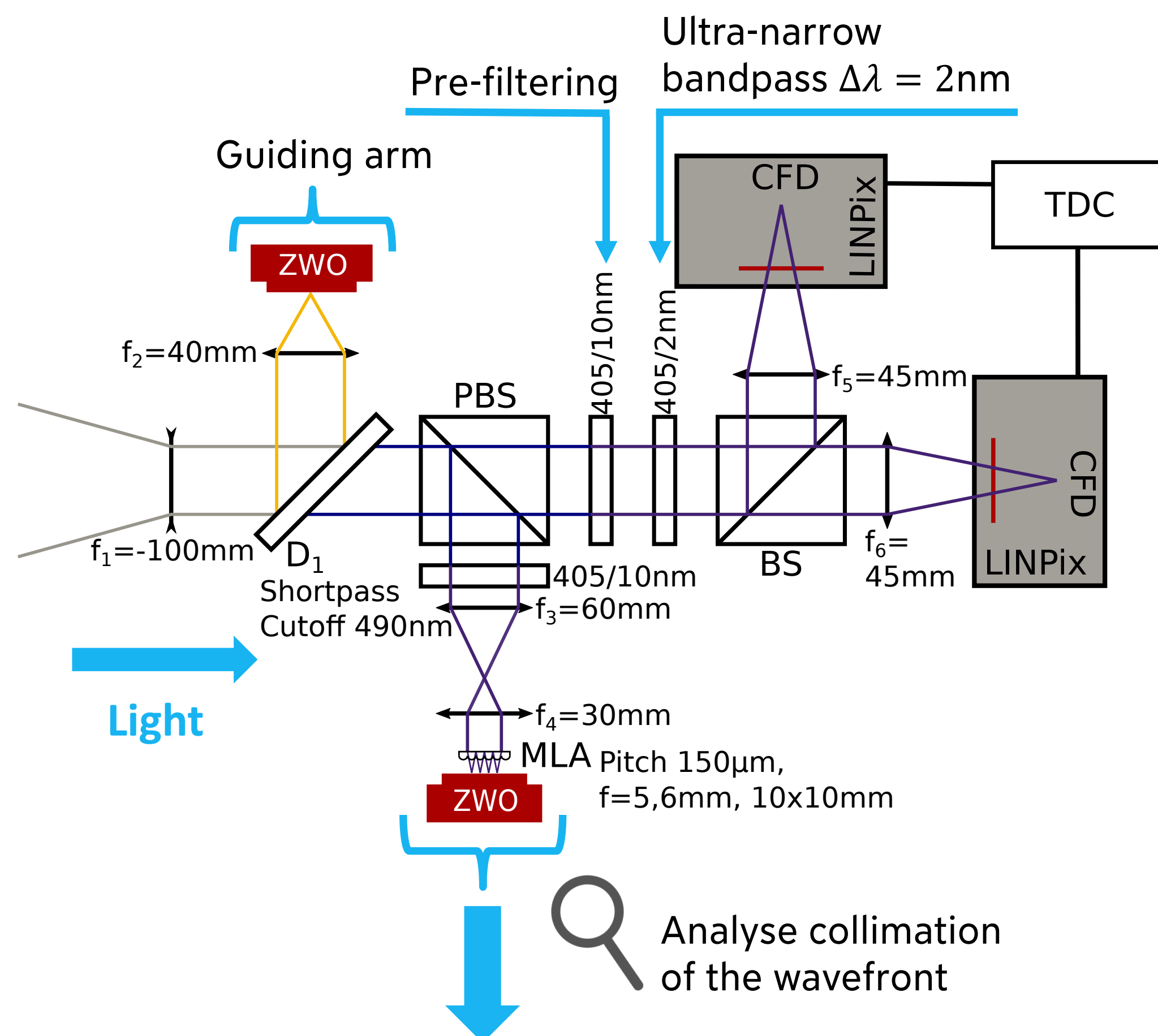
Zernike coefficient

$$W(x, y) = \sum_{i=0}^N a_i Z_i(x, y)$$

Total wavefront distortion

i-th Zernike polynomial

OPTICAL SETUP



Analyse collimation of the wavefront

SHACK-HARTMANN ARM

Why is it needed?

- 2nm filter improves contrast for $g^{(2)}$ measurements
- wavefront needs to be collimated
- for distorted wavefront filtering fails

How does it work?

- beam is spatially reduced to fit camera sensor
- microlens array (MLA) creates spot pattern
- spot deviations indicate distortions

ZERNIKE POLYNOMIALS

- spot deviations are mapped to polynomials
- any polynomial set can be used
- choose Zernike polynomials as they are orthogonal and represent common aberrations
- cartesian coordinates need to be normalized to unit circle

Zernike Term	Zernike Polynomial	Name	Normalization Factor
Z_0	1	Piston	1
Z_1	$\rho \cos \theta$	X-Tilt	2
Z_2	$\rho \sin \theta$	Y-Tilt	2
Z_3	$2\rho^2 - 1$	Defocus	$\sqrt{3}$